



## Real Vibrations Simulation Tools

## **USER MANUAL**

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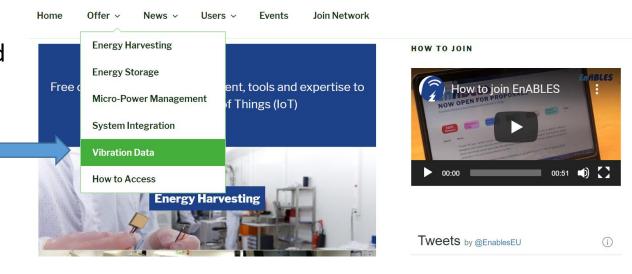






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- Users are not required to register to view basic information about the dataset, but to download raw data a login is required.
- Once registered, users are able to log in, to access data and to download as much time series data as required without restrictions.









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#### **Energy Harvesting DATABASES**

The following data/tools are currently available:

- Energy Harvesting Data Repository (Univ. of Southampton)
- Real Vibrations Database (Univ. of Perugia)
- Simulation Tool for Energy Harvesting Applications (Univ. of Perugia)

To access this data, all you have to do is register by filling the <u>EnABLES Enquiry</u> Form, selecting **Database** as the offer of interest.

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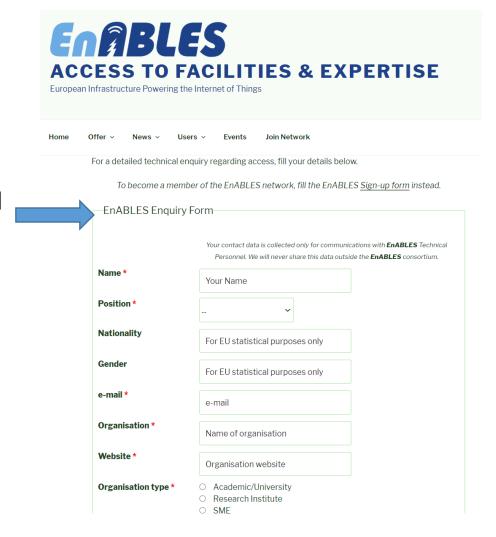
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Once you have registered, please click here to access the data repository.





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- From the access webpage the users can choose the vibrations database developed by University of Southampton or Real Vibrations Database from University of Perugia.
- Now there is the direct link to the simulation tools totally free-of-charge for the EnABLES users.
- Currently, two main simulators are available: the general transduction-independent vibration energy harvester and piezoelectric vibration harvester. However, thi toolset is under development so that new tools will be available soon!



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Database access interface

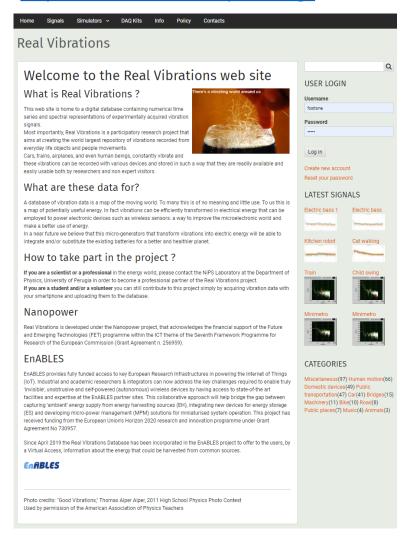






- The RealVibration database by NiPS/UNIPG is contains numerical time series and spectral representations of experimentally acquired vibration signals.
- Most importantly, Real Vibrations is a participatory research project so that under request o the administrator users can upload their recorded vibrations from everyday life.
- It includes: cars, trains, airplanes, and even human beings, recorded with various devices and readily available and easily usable both by researchers and non expert visitors.

#### https://realvibrations.nipslab.org/



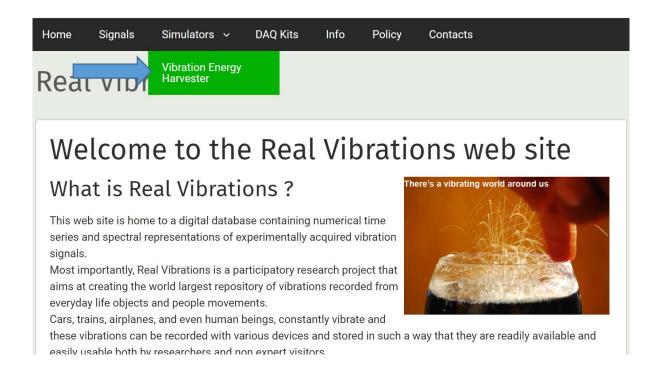




- SIMULATION TOOLSET
  - Vibration Energy Harvester

https://realvibrations.nipslab.org/node/1099

Piezoelectric Energy Harvester

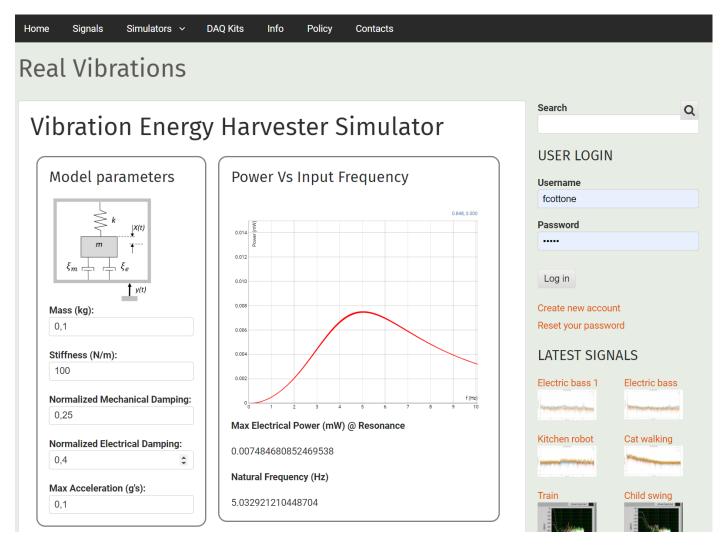






https://realvibrations.nipslab.org/node/1099

- The first tool is a simulator of transduction-independent vibration harvester based on the theoretical model of William and Yates <a href="https://doi.org/10.1016/0924-4247(96)80118-X">https://doi.org/10.1016/0924-4247(96)80118-X</a>.
- The vibration harvester is a springmass-damped resonant oscillator in which the energy conversion is accounted by the electrical damping.
- The user simply provides the inertial mass m, the spring equivalent stiffness k, the normalized mechanical and electrical damping e and the maximum input acceleration.









#### Theoretical model

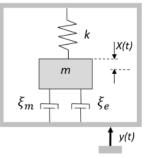
- The Newton's motion equation for an inertial generator is the following:
- where, the mechanical damping ratio is related to the mechanical and electric viscous damping, with  $k_t^2$  and  $R_l$  being respectively the electro-mechanical transduction coefficient and the resistive load,
- by assuming a simple Harmonic excitation of input frequency  $f=\omega/2\pi$  and phase  $\phi=0$ ,
- the electrical power versus input vibration frequency is then calculated with the following expression:

$$m\ddot{z}(t) + (d_m + d_e)\dot{z}(t) + kz(t) = -m\ddot{y}(t)$$

$$\zeta_m = \frac{d_m}{2m\omega_n}, \qquad \qquad \zeta_e = \frac{k_t^2}{2m\omega_n R_l}$$

$$\ddot{y}(t) = Y_0 \sin(\omega t + \phi)$$

$$P_e(\omega) = \frac{m\zeta_e \left(\frac{\omega}{\omega_n}\right)^3 \omega^3 Y_0^2}{\left[1 - \left(\frac{\omega}{\omega_n}\right)^2\right]^2 + \left[2(\zeta_e + \zeta_m)\frac{\omega}{\omega_n}\right]^2}$$



Mass (kg):

0,1

Stiffness (N/m):

100

**Normalized Mechanical Damping:** 

0,25

**Normalized Electrical Damping:** 

0,4

Max Acceleration (g's):

0,1







#### Theoretical model

- The Newton's motion equation for an inertial generator is the following:
- where, the mechanical damping ratio is related to the mechanical and electric viscous damping, with  $k_t^2$  and  $R_l$  being respectively the electro-mechanical transduction coefficient and the resistive load,
- by assuming a simple Harmonic excitation of input frequency  $f=\omega/2\pi$  and phase  $\phi=0$ ,
- At resonance for  $\omega = \omega_n$ , the maximum power is given by the following formula.
- The power can be maximized when the condition is verified

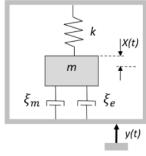
$$m\ddot{z}(t) + (d_m + d_e)\dot{z}(t) + kz(t) = -m\ddot{y}(t)$$

$$\zeta_m = \frac{d_m}{2m\omega_n}, \qquad \qquad \zeta_e = \frac{k_t^2}{2m\omega_n R_l}$$

$$\ddot{y}(t) = Y_0 \sin(\omega t + \phi)$$

$$P_{max}(\omega_n) = \frac{1}{4} m \omega_n^3 Y_0^2 \frac{\zeta_e}{(\zeta_e + \zeta_m)}$$

$$\zeta_e = \zeta_m$$



Mass (kg):

4			

Stiffness (N/m):

10	

**Normalized Mechanical Damping:** 

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**Normalized Electrical Damping:** 

0,4
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Max Acceleration (g's):

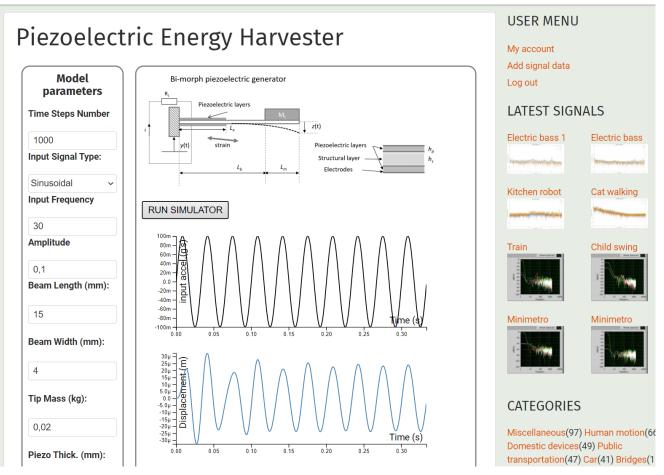
0,1





https://realvibrations.nipslab.org/node/1100

- The second tool regards the simulation of a vibrational energy harvester based on a piezoelectric bi-morph cantilever.
- The web application performs a numerical integration of the dynamical equations of the piezoelectric bi-morph based on theoretical model of Roundy, S., & Wright, P. K. (2004). <a href="https://doi.org/10.1088/0964-1726/13/5/018">https://doi.org/10.1088/0964-1726/13/5/018</a>; Cottone F. et al. (2015). <a href="https://doi.org/10.1140/epjst/e2015-02593-5">https://doi.org/10.1140/epjst/e2015-02593-5</a>
- The user can select any signal coming from the database (even stochastic). The integration is performed with modified Euler-Maruyama with predictor-corrector algorithm.







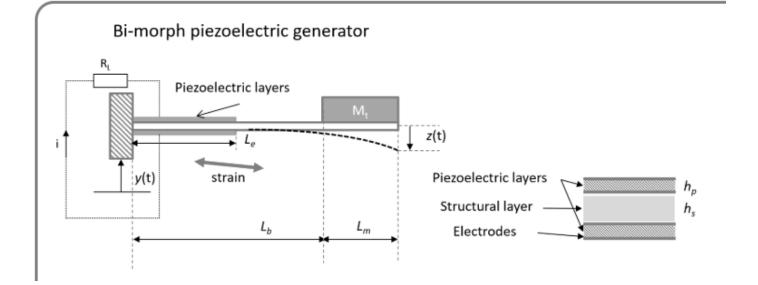
#### **INPUT PARAMETERS**

https://realvibrations.nipslab.org/node/1100

Model parameters
Time Steps Number
1000
Input Signal Type:
Database Signal 🗸
Database Signal
Car (30 s) ~
Input Frequency
30
Amplitude
0,1
Beam Length (mm):

Beam Width (mm):
4
Tip Mass (kg):
0,02
Piezo Thick. (mm):
0,2
Struct. Thick. (mm):
0,1
Mech. Damping Ratio:
0,03
Load Resist. (ohm):
100e3

#### **GENERATOR MODEL**







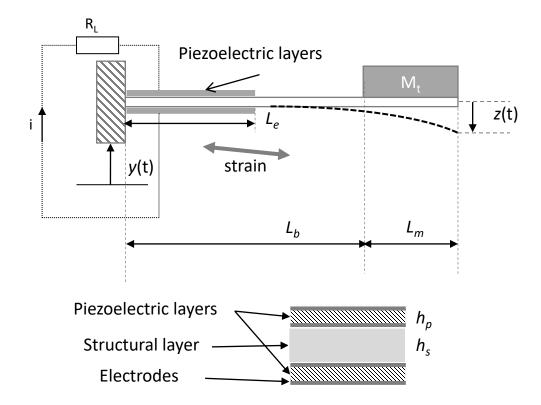
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 The system of governing equations of the main model are derived from the Newton's and Kirchhoff's laws as follows:

$$m\ddot{z}(t) + 2\zeta_m \omega_n \dot{z}(t) + kz(t) + k_v V(t) = -m\ddot{y}(t)$$
 
$$\dot{V}(t) + \frac{1}{R_l C_p} V(t) = k_c \dot{z}(t)$$

• where the  $k_v, k_c$  and  $\mathcal{C}_p$  represent the electro-mechanical transduction coefficient, the velocity-voltage coefficient and the equivalent capacitance of the piezoelectric beam. These parameters are derived from the particular geometry and electrical properties of the piezoelectric generator: such as beam length, width, thickness and piezoelectric constant of the material.

### Bi-morph piezoelectric generator







https://realvibrations.nipslab.org/node/1100

• The **dependent parameters** are derived from the **input parameters** as the paper of Roundy [1] and Cottone [2].

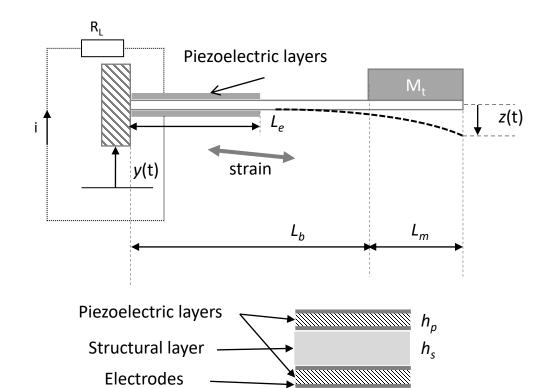
$$k_v = k d_{31}/h_p k_2$$
 Electro-mechanical transduction coefficient

$$k_c = 2h_p d_{31} E_p k_2/(ae_p)$$
 Voltage to velocity coefficient

$$k_1 = \frac{2I}{b(2L_h + L_m - L_e)}$$
 Average strain to input force

$$k_2 = \frac{3b(2L_b + L_m - L_e)}{L_b^2 \left(2L_b + \frac{3}{2}L_m\right)}$$
 Average strain to vertical displacement

### Bi-morph piezoelectric generator





<sup>[1]</sup> Roundy, S., & Wright, P. K. (2004). <a href="https://doi.org/10.1088/0964-1726/13/5/018">https://doi.org/10.1088/0964-1726/13/5/018</a>

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 The dependent parameters are derived as the paper of Roundy [1] and Cottone [2].

$$I=2\left(rac{w_bh_p^3}{12}+w_bh_pb^2
ight)+rac{1}{12}\left(rac{E_p}{E_{sh}}w_bh_{sh}^3
ight)$$
 Beam area inertia moment

$$K = E_p k_2 k_1$$
 Equivalent spring constant of the beam

$$C_p = rac{a^2 e_p w_b L_e}{2h_p}$$
 Equivalent capacitance of piezoelectric beam

 $a=1\ or\ 2$  It is equal to 1 for series and 2 for parallel connection of the bi-morph

$$b = \frac{h_p}{2} + \frac{h_{sh}}{2}$$
 distance between structural and piezoelectric layer

- [1] Roundy, S., & Wright, P. K. (2004). <a href="https://doi.org/10.1088/0964-1726/13/5/018">https://doi.org/10.1088/0964-1726/13/5/018</a>
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